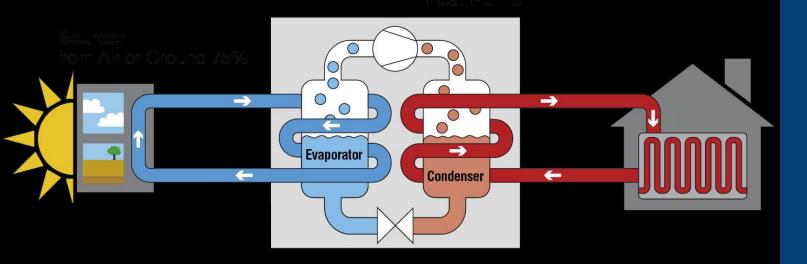
Assessing the impact of cold plumes from air source heat pumps

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Introduction

- Air Source Heat Pump configuration
- Model set up
 - ADMS 5
 - GASTAR
 - Meteorological data
- Some results
- Tentative conclusions
- Further work

CERC was approached to model the impact of plumes of cold air from an array of air source heat pumps

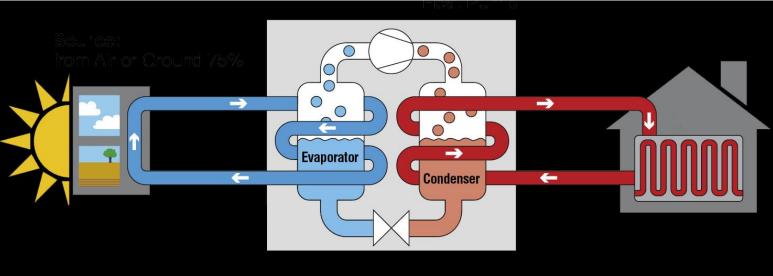
- Energy Centre for district heating scheme
- Concern regarding potential impact of cold air
 - on surrounding vegetation?
 - on railway tracks?
- Emitted air ~4 °C colder than ambient
- Dense plume compared to ambient air: use GASTAR?





How does an Air Source Heat Pump (ASHP) work?

- An ASHP works like a refrigerator in reverse. It consists of an evaporator, a compressor and a condenser.
- Heat from the ambient air, drawn in by a fan, is absorbed into a fluid at low temperature.
- The compressor increases the temperature of the fluid and transfers that heat to the building.



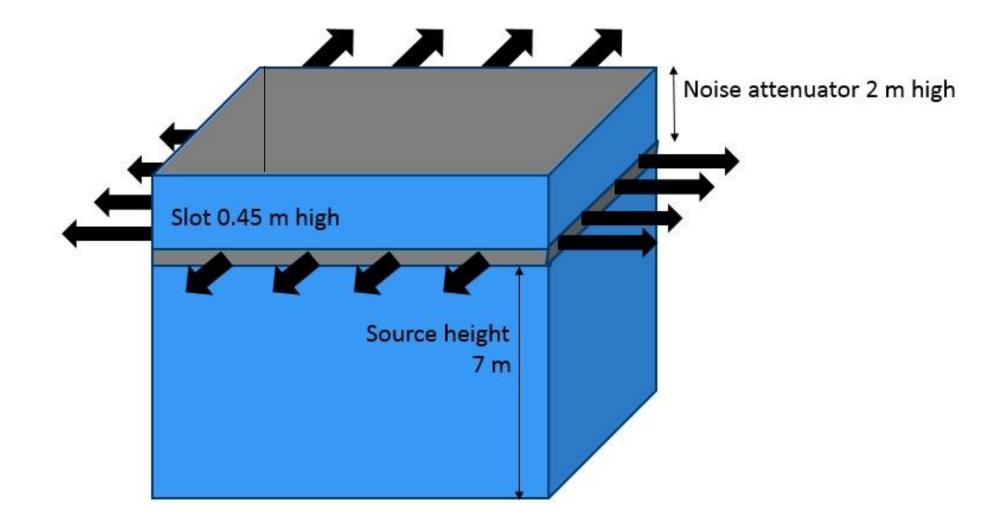


Air Source Heat Pump configuration

- 16 unit air source heat pump (ASHP) array
- One unit emits 30 kg/s (25 m³/s) of cold air ~4 °C below ambient
- Located on 7 m high building, dimensions 18 m by 17 m
- Noise attenuation screen extends a further 2 m upwards
- Cold air emitted via horizontal slot, vertical dimension 0.45 m, at height of 7 m, along all four sides
- Cold air emitted over total area 31.5 m²



Schematic of ASHP configuration





Model set-up

- Modelled as a horizontal jet in both ADMS 5 and GASTAR
- Modelled emissions from one side of the building only
- Single jet modelled to represent a single unit / combined emissions along the whole of one side, because:
 - Multiple plumes in ADMS 5 don't interact
 - GASTAR can only model a single source
- Total area of aperture was used to determine representative source diameter and efflux velocity
- Assumed ambient temperature 12 °C, plume temperature 8 °C

- Building effects cannot be modelled with jets
 - Considered relatively unimportant due to high horizontal momentum: 12.7 m/s
 - See CERC's ADMLC report on non-point sources
 <u>https://admlc.files.wordpress.com/2014/05/fm1019_cerc_admlc_final_mar16.pdf</u>
- Included .aai file to request temperature output
 - Short term temperature output for downstream jets'



Model set-up for GASTAR

- Mass flow (not volume flow) specified
- User defined source material 'dry air'

🛃 GASTAR (3.2) : P:\FM\FM1280_SustEnergy_cold	\Runs\\Eight_D5.Gl	PL	- • •						
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Meteorology Source	Complex Effects	Output	Graphics						
C Source Material									
Dry air	🗌 🔿 From Datab	Fd	lit User Data						
	Oser Define	d <u> </u>							
Release <u>T</u> ype									
C Instantaneous		Isotherm	al Release						
C Continuous		T Thermal	Release						
C Time Varying		A Aerosol							
 Gas or Liquid Jet 									
Source Details									
Source Location TQ301799 (UK)	Change R	elease Start (UTC) 12:00) 27 Jan 2020 💌						
Diameter (m) 3.21									
Mass Flux (kg/s) 240									
Hazardous Fraction (mol/mol) 1		Height	(m) 7						
Temperature (K) 281 Azimuthal Angle (*)									
		Elevation Angle	e (*) 0						
Jet diameter or jet pseudo diameter Min: 0.01 Max: 1000									

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• HSE Safety Report Assessment Guide (SRAG) guidance for a dense gas release:

"D5 weather conditions occur frequently in the UK and should be used to calculate the hazard range for daytime releases... Dispersion is reduced under stable atmospheric conditions, hence F2 weather, which characterises night time conditions, generally produces the greatest hazard range".

- Standard practice to include these conditions for risk assessment scenarios:
 - D5 (category D with wind speed 5 m/s): prevailing daytime conditions in the UK
 - F2 (category F with wind speed 2 m/s): less common, occurring 10% of the time



ADMS 5 meteorological data screen

- D5 and F2 represented using data from <R91A-G.met>
- Jet pointing downstream

Surface heat flux variables O year/day/time/cloud cover (yr/dy/hr/oktas) (• surface sensible heat flux, (W/m²)					Met. parameters to be entered ✓ boundary layer height, h (m) ✓ surface temperature, TOC (°C) ✓ lateral spread (meandering), (°)	
<u>N</u> ew	<u>D</u> elete	1			☐ relative humidity (%)	
Wind speed (m/s) 5 2 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	Wind angle (*) 0 0	Surface heat flux (W/m²) -6	Boundary layer height (m) 800 100 100	Surface temp. (°C) 12 12 12		
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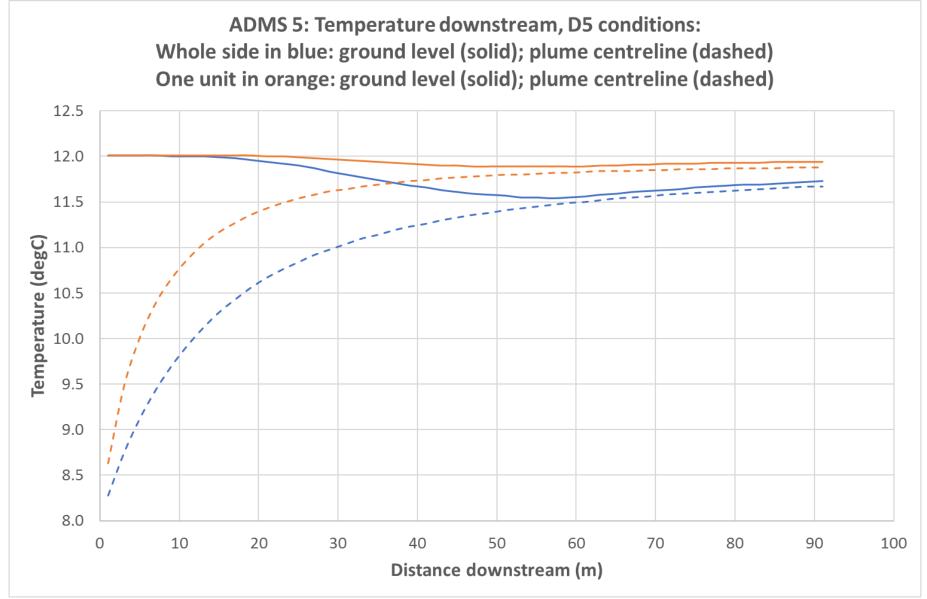
GASTAR meteorological data screen

- D5 and F2 set up as standard conditions in GASTAR
- Jet pointing downstream

😖 GASTAR (3.2) : P:\FM\FM1280_SustEnergy_cold\Runs\\Eight_D5.GPL 🛛 👘 🗐						
<u>File R</u> un! <u>H</u> elp						
Meteorology	Source	Complex Effects	Output	Graphics		
Wind Spe	ed (m/s)	5	Air Temperature (K)	285		
Wind Speed He	eight (m)	10	Surface Temperature (K)	285		
Wind Dire	ction (*)	0 .	Atmospheric Pressure (mb)	1013		
Roughness Le	ngth (m)).3	Relative Humidity (%)) 70		
PG / Monin-Obukhov De	ategories	ου [se Monin-Obukhov Length			
PGC: 'D' means neutral conditions			Min:	A Max: G		



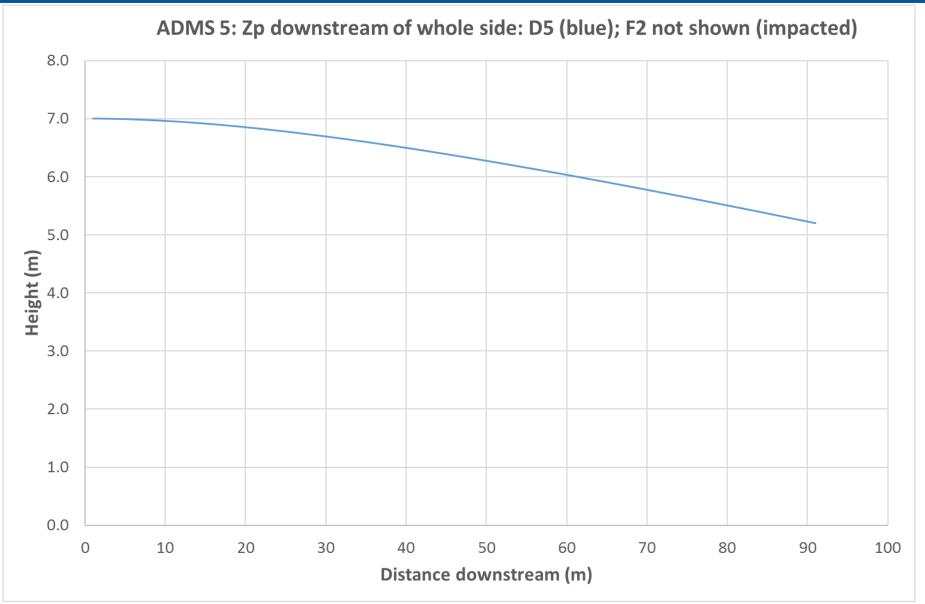
Downstream temperatures, ADMS 5



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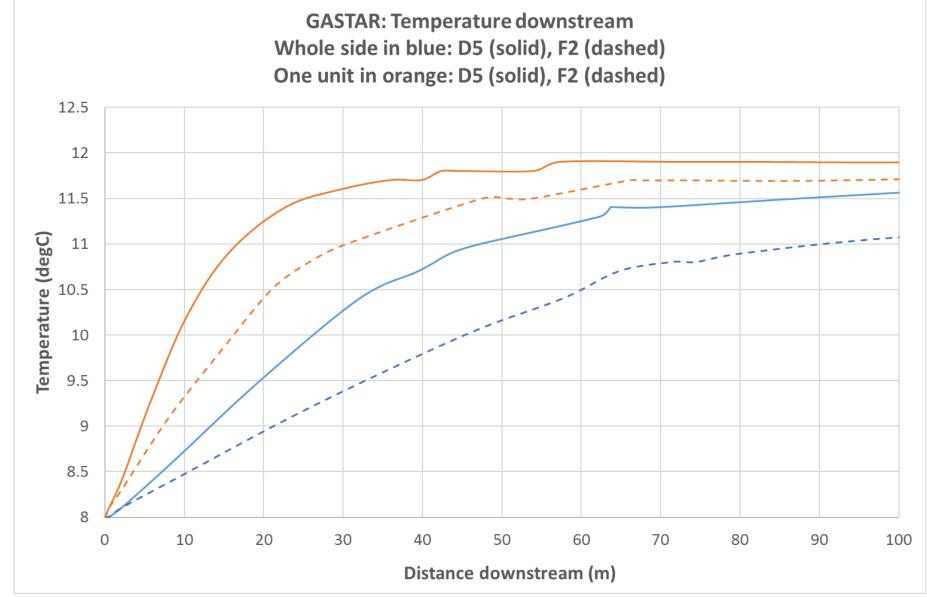
Plume centreline height, ADMS 5



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Downstream temperatures, GASTAR



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- Results indicate that ground level temperature downwind of the release will be no more than 1 °C lower than ambient
- i.e. by the time the plume reaches ground level, the plume temperature has increased to at least 11 °C
- ADMS 5 indicates maximum ground level temperature deficit at around 60 m downstream



Further work

- Neither ADMS 5 or GASTAR can consider all aspects of the problem
 - ADMS can treat multiple sources
 - GASTAR can model dense gas effects at the ground
- Model for a range of ambient conditions (nearby meteorological station)
- Produce contour plots of temperature deficit
- Generate results at different heights above ground level
- Meteorological conditions of most interest light wind, stable stratification are the most difficult to model accurately, so there will be uncertainty
- To give confidence, compare rate of cooling due to ASHPs with typical rates of radiative cooling/heating and turbulent heat fluxes



Any questions?

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